Direct Power Control: Theories and Applications

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Key References

[1] S. Yan, Y. Yang, S. Y. Hui and F. Blaabjerg, "A Review on Direct Power Control of Pulsewidth Modulation Converters," in *IEEE Trans. on Power Electron.*, vol. 36, no. 10, pp. 11984-12007, Oct. 2021.

[2] S. Yan, J. Chen, M. Wang, Y. Yang and J. M. Rodriguez, "A Survey on Model **Predictive Control of DFIGs in Wind Energy Conversion Systems**," in *IEEE Trans.* on Power Electron. (under review).

[3] S. Yan, et al, "A General Space Vector Modulation Method of Three-Phase Multilevel Converters," in *IEEE Trans. on Power Electron. (under review)*.



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Introduction

Voltage-Oriented Control (VOC)

Direct Power Control (DPC)^[1]







Introduction

Comparison of Two Mainstream Controls^[1]

VOC	DPC			
Average Model	Discrete Model			
Frame Transformation (<i>d-q</i> or α - β)	Optional			
Double Loops (Current and Voltage)	Single Loop or Nonlinear logics			
Linear Controller (PI or PR)	Optional			
Pulsewidth Modulation	Optional			



Space Vectors (2-Level Converters) [3]





Space Vectors (n-Level Converters)^[3]



[3] S. Yan, et al, "A General Space Vector Modulation Method of Three-Phase Multilevel Converters," in *IEEE Trans. on Power Electron. (under review).*



Power Derivative and Space Vectors

Instantaneous
Power
$$\mathbf{S} = \frac{3}{2} (\mathbf{e} \cdot \mathbf{i}^*)$$



Power Derivative and Space Vectors





Power Derivative and Space Vectors





Power Derivative and Space Vectors





- Power Derivative and Space Vectors
 - 2. DFIG





The Use of Power Derivative





The Iteration of Power Derivative





Control Formation

	q	The Sector Number					
p		1	2	3	4	5	6
1	1	V4	V5	V6	V1	V2	V3
1	\checkmark	V6	V1	V2	V3	V4	V5
\checkmark	1	V2	V3	V4	V5	V6	V1
1	1	V1	V2	V3	V4	V5	V6

(One example)



- 1. Angle Calculator
- 2. Power Error Calculator
- 3. Switching Table



•

- Improvements (Accuracy and Ripple Reduction) ^[1]
 - Vector redundance
 - Sector refinement





Output Regulation Subspace Analysis

• Dynamic table



Improvements (Accuracy and Ripple Reduction) ^[1]



Removal of false duty cycles^[4]

[4] S. Yan, J. Chen, T. Yang, and S. Y. Hui, "Improving the Performance of Direct Power Control Using Duty Cycle Optimization," *IEEE Trans. Power Electron.*, vol. 34, no. 9, pp. 9213-9223, Sept. 2019.



Finite-Control-Set Predictive DPC (FCS-P-DPC)

 $\frac{d\mathbf{S}}{dt} = f(\mathbf{v}) \longrightarrow \text{Prediction:} \quad \mathbf{S}_i(k+1) = \mathbf{S}(k) + T_s \cdot \frac{d\mathbf{S}}{dt}\Big|_{\mathbf{v}_i}, i = 1, 2, \dots n$

Objective Function: $obj = \left\| \mathbf{S}_{ref} - \mathbf{S}_i \left(k + 1 \right) \right\|_m^m$

Optimization: $\mathbf{v}_{opt} = \min(obj)$



Single-Vector FCS-P-DPC



- Power error prediction: power derivative, power prediction, error calculation
- 2. The selection of the optimal vector



Multi-Vector FCS-P-DPC

1. Duty cycle calculation

$$\mathbf{y}(k+1) = \mathbf{y}(k) + \sum_{j=1}^{h} \left(\frac{d\mathbf{y}(t)}{dt} \Big|_{u(t)_{j}} \cdot t_{j} \right)$$

$$\mathbf{e}(k+1) = \mathbf{y}^{ref}(k+1) - \mathbf{y}(k+1)$$

$$\begin{bmatrix} \frac{\partial \mathbf{e}(k+1)}{\partial t_{1}} = 0 \\ \dots \\ \frac{\partial \mathbf{e}(k+1)}{\partial t_{h}} = 0 \end{bmatrix}$$

$$\mathbf{y}^{ref}(k+1) - \mathbf{y}(k+1)$$

2. An example of three-vector's approach



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Multi-Vector FCS-P-DPC

3. Control Formation



- Power error prediction: power derivative, power prediction, error calculation
- 2. The selection of the optimal vectors
- 3. Duty cycle calculation



- FCS-P-DPC Improvements (Accuracy and Ripple Reduction) ^[1]
 - Two-vector approaches: Active plus zero, two active vectors
 - Two-step prediction





- FCS-P-DPC Improvements (Accuracy and Ripple Reduction)^[1]
 - Three-vector approaches: 3+3



• Low-complexity evaluation: negative conjugate of complex power



Deadbeat P-DPC

 $\frac{d\mathbf{S}}{dt} = f(\mathbf{v}) \longrightarrow \text{Discretization:} \quad \frac{\mathbf{S}(n+1) - \mathbf{S}(n)}{T_s} = f(\mathbf{v})$ $\text{Inverse}_{\text{Function:}} \quad \mathbf{v} = f^{-1} \left(\frac{\mathbf{S}(n+1) - \mathbf{S}(n)}{T_s} \right)$ $\text{Absolute}_{\text{Solution:}} \quad \mathbf{v}_{ref} = f^{-1} \left(\frac{\mathbf{S}_{ref} - \mathbf{S}(n)}{T_s} \right)$



Deadbeat P-DPC



- 1. Deadbeat calculation: Inverse function
- 2. Space vector modulation



- Deadbeat P-DPC Improvements: Robustness^[1]
 - Influence of Inductance Variation



Solutions:

- 1. Ohm' theory
- 2. Constant voltage magnitude
- 3. Continuity of line current and DC voltage
- 4. Least-square evaluation



Implementation Issues

• Sampling delay

Two-step prediction; Incorporation of delay in the discrete model Observer-based methods

• Objective functions

l₁-norm, l₂-norm, or others;
Additional control constraints;
Weighting factors (weight-factor-less methods)



Other Nonlinear DPCs

Sliding Mode DPCs



- 1. Sliding mode algorithm: equivalent function
- 2. Space vector modulation



Other Nonlinear DPCs

Super Twisting DPCs





DPC with Linear Controllers

 \succ α-β frame





DPC with Linear Controllers

d-q frame^[5]



- 1. Linear controller and cancellation terms
- 2. Inverse Clarke transformation
- 3. Modulation

[5] Y. Gui, et el, "Improved Direct Power Control for Grid-Connected Voltage Source Converters," *IEEE Trans. Ind. Electron.*, vol. 65, no. 10, pp. 8041-8051, Oct. 2018.



Sensorless DPCs

Source Voltage Estimation

$$\frac{d\mathbf{i}}{dt} = \frac{1}{L} \left(\mathbf{e} - \mathbf{v} - r\mathbf{i} \right) \qquad \mathbf{e} = \mathbf{v} + r\mathbf{i} + L \frac{d\mathbf{i}}{dt}$$

Virtual Flux and More

$$\mathbf{e} = \mathbf{v} + r\mathbf{i} + L\frac{d\mathbf{i}}{dt} \implies \int \mathbf{e} = \int \left(\mathbf{v} + r\mathbf{i} + L\frac{d\mathbf{i}}{dt}\right) \implies \mathbf{\psi} = \int \mathbf{v} + L\mathbf{i}$$



Sensorless DPCs

Source Voltage Estimation

$$\frac{d\mathbf{i}}{dt} = \frac{1}{L} \left(\mathbf{e} - \mathbf{v} - r\mathbf{i} \right) \quad \blacksquare \quad \mathbf{e} = \mathbf{v}(k) + r\mathbf{i} + L \frac{\mathbf{i}(k) - \mathbf{i}(k-1)}{t_s}$$

Virtual Flux and More

$$\mathbf{e} = \mathbf{v} + r\mathbf{i} + L\frac{d\mathbf{i}}{dt} \implies \int \mathbf{e} = \int \left(\mathbf{v} + r\mathbf{i} + L\frac{d\mathbf{i}}{dt}\right) \implies \mathbf{\psi} = \int \mathbf{v} + L\mathbf{i}$$



Sensorless DPCs

Virtual Flux and More



- 1. Issues of pure integrators: dc drifting and saturation
- 2. Improvements:
 - Frequency-adaptive integrators
 - First-order low pass filters (FOLP)
 - Second-order general integrators (SOGI)
 - Observer-based estimator: SMO, LO, Kalman filter.



Revisit of Instantaneous Power Theory

$$\mathbf{S} = \frac{3}{2} \left(\mathbf{e} \cdot \mathbf{i}^* \right)$$

$$\mathbf{i} = \mathbf{i}^+ + \mathbf{i}^- = I^+ e^{j\omega t} + I^- e^{-j\omega t}$$

$$\begin{cases} p = P_0 + P_{c2} \cos(2\omega t) + P_{s2} \sin(2\omega t) \\ q = Q_0 + Q_{c2} \cos(2\omega t) + Q_{s2} \sin(2\omega t) \end{cases}$$
6 power terms with 4 variables.



Extended Power Definitions

$$P_{s}^{ext} = -\frac{3}{2} \operatorname{Im} \left(\mathbf{i}^{*} \cdot \mathbf{e}^{'} \right)$$

$$Q_{s}^{ext} = \frac{3}{2} \operatorname{Re} \left(\mathbf{i}^{*} \cdot \mathbf{e}^{'} \right)$$

$$Q_{s}^{ext} = \frac{3}{2} \operatorname{Re} \left(\mathbf{i}^{*} \cdot \mathbf{e}^{'} \right)$$

$$Q_{s}^{ext} = \frac{3}{2} \operatorname{Re} \left(\mathbf{i}^{*} \cdot \mathbf{e}^{'} \right)$$

$$Q_{s}^{ext} = Q_{0}^{ext} + Q_{s2}^{ext} \sin(2\omega t) + Q_{c2}^{ext} \cos(2\omega t)$$

$$q = Q_{0} + Q_{c2} \cos(2\omega t) + Q_{s2} \sin(2\omega t)$$

$$q = Q_{0} + Q_{c2} \cos(2\omega t) + Q_{s2} \sin(2\omega t)$$

$$Q_{s2}^{ext} = Q_{c2} \cos(2\omega t) + P_{s2} \sin(2\omega t)$$

$$Q_{s2}^{ext} = Q_{c2} \cos(2\omega t) + P_{s2} \sin(2\omega t)$$

$$Q_{s2}^{ext} = P_{c2} - Q_{c2}^{ext} = -P_{s2}$$



Power Ripple Compensation (classic definition)



- 1. Sequence detection;
- 2. Ripple calculation, selective control targets;
- 3. DPC strategies.



Power Ripple Compensation (extended definition)



- 1. Extended power calculation;
- 2. DPC strategies.



Mainstream Applications

PWM Converters



Linear DPC Decoupled power control

> PR control for harmonic compensation

Grid voltage modulated DPC





Mainstream Applications

Doubly Fed Induction Generators





Mainstream Applications

- Multilevel Converters
- Active Power Filters
- Single-Phase Converters









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